

# Lecture 15 – Equipment models

Purdue ME 200, Thermodynamics I

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# Outline

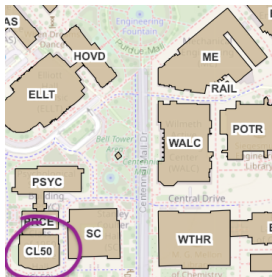
Exam reminders

Nozzles and diffusers

Turbines, compressors and pumps

# When and where is exam #1?

- 6:30–7:30 PM in CL-1950 room 224 on Thursday, February 16



- no class Friday, February 17
- homework 14-16 due 11:59 PM Monday, February 20

## What does exam #1 cover?

- lectures 1-12 and homework 1-13
- 1 'concepts' problem, 2 homework-style problems
- closed book, closed notes
- we'll provide equation sheet and any necessary tables
- don't interpolate tables; just use closest data point

## Other exam #1 logistics

- practice problems & exam are on Brightspace
- arrive 10-15 minutes early
- bring pencils, eraser, scientific calculator
  - ◇ Texas Instruments: TI-30X, TI-36X
  - ◇ Cassio: fx-115 or fx-991
- exams 1, 2 and 3 are each 20% of course grade
- final exam is 25%

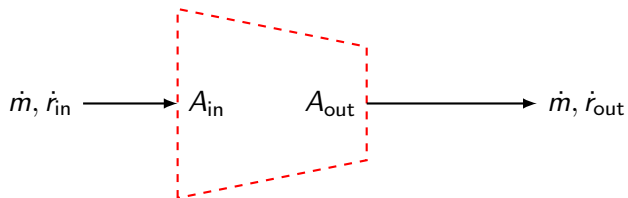
# Outline

Exam reminders

**Nozzles and diffusers**

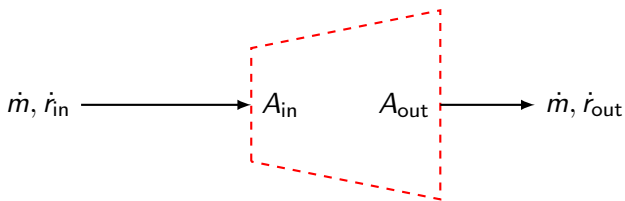
Turbines, compressors and pumps

# Nozzles



- nozzles increase flow velocity:  $\dot{r}_{out} > \dot{r}_{in}$
- and decrease pressure:  $p_{out} < p_{in}$

# Diffusers



- diffusers are 'backwards nozzles'
- they decrease flow velocity:  $\dot{r}_{out} < \dot{r}_{in}$
- and increase pressure:  $p_{out} > p_{in}$



# Typical assumptions for nozzles and diffusers

- steady state
- one-dimensional flow
- no change in PE
- no boundary/shaft/electrical/etc. work
- under these assumptions, diffusers and nozzles satisfy

$$\dot{m} \left[ \frac{1}{2}(\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) + h_{\text{in}} - h_{\text{out}} \right] = -\dot{Q}$$

- if  $\dot{Q} = 0$  (good insulation or small  $\Delta T$  across boundary), then

$$\frac{1}{2}(\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) = h_{\text{out}} - h_{\text{in}}$$

## Example

Consider a well-insulated diffuser with  $0.02 \text{ m}^2$  inlet cross-sectional area. Steam enters at  $300 \text{ m/s}$ ,  $5 \text{ bar}$  and  $180 \text{ }^\circ\text{C}$ . Steam exits at  $7 \text{ bar}$  and  $200 \text{ }^\circ\text{C}$ .

- (a) What is the exit velocity?
- (b) What is the outlet cross-sectional area?

# Given and find

- **given:**

- ◇  $A_{\text{in}} = 0.02 \text{ m}^2, \dot{r}_{\text{in}} = 300 \text{ m/s}$

- ◇  $p_{\text{in}} = 5 \text{ bar}, T_{\text{in}} = 180 \text{ }^\circ\text{C}$

- ◇  $p_{\text{out}} = 7 \text{ bar}, T_{\text{out}} = 200 \text{ }^\circ\text{C}$

- **find:**

- (a)  $\dot{r}_{\text{out}}$

- (b)  $A_{\text{out}}$

# Assumptions and basic equations

- **assume:**

- ◇ steady state
- ◇ one-dimensional flow ( $\dot{m} = \rho A \dot{r}$ )
- ◇ no change in PE ( $z_{\text{out}} = z_{\text{in}}$ )
- ◇ no boundary/shaft/electrical/etc. work ( $\dot{W} = 0$ )
- ◇ well-insulated ( $\dot{Q} = 0$ )

- **basic equations:**

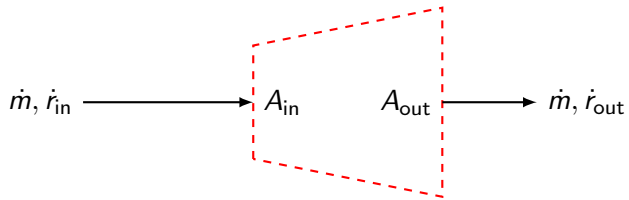
- ◇ steady-state, single-input single-output CoM:

$$\dot{m}_{\text{in}} = \dot{m}_{\text{out}}$$

- ◇ steady-state, single-input single-output 1st law:

$$\dot{m} \left[ \frac{1}{2} (\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) + g(z_{\text{in}} - z_{\text{out}}) + h_{\text{in}} - h_{\text{out}} \right] = \dot{W} - \dot{Q}$$

# System diagram



## Solution to part (a)

- from the 1st law for open systems in steady state,

$$\frac{1}{2}(\dot{i}_{in}^2 - \dot{i}_{out}^2) = h_{out} - h_{in}$$

$$\Rightarrow \dot{i}_{out} = \sqrt{\dot{i}_{in}^2 - 2(h_{out} - h_{in})}$$

- superheated steam tables give specific enthalpies:

Temp. (C)	Volume (m <sup>3</sup> /kg)	Internal Energy (kJ/kg)	Enthalpy (kJ/kg)	Entropy (kJ/kg/K)	Volume (m <sup>3</sup> /kg)	Internal Energy (kJ/kg)	Enthalpy (kJ/kg)	Entropy (kJ/kg/K)
	p = 5.0 bar = 0.50 MPa, T <sub>sat</sub> = 151.83°C				p = 7.0 bar = 0.70 MPa, T <sub>sat</sub> = 164.95°C			
Sat.	0.37481	2560.7	2748.1	6.8207	0.27277	2571.8	2762.8	6.7071
180	0.40466	2610.1	2812.4	6.9673	0.28476	2600.0	2799.4	6.7893
200	0.42503	2643.3	2855.8	7.0610	0.30000	2635.3	2845.3	6.8884

## Solution to part (a) (continued)

- plugging in numbers,

$$\begin{aligned} \dot{r}_{\text{out}} &= \sqrt{\dot{r}_{\text{in}}^2 - 2(h_{\text{out}} - h_{\text{in}})} \\ &= \sqrt{(300\text{m/s})^2 - 2(2845\text{kJ/kg} - 2812\text{kJ/kg})(1000\text{J/kJ})} \\ &= 155.6\text{m/s} \end{aligned}$$

- units check:  $\text{J/kg} = \text{N m/kg} = (\text{kg m/s}^2)\text{m/kg} = \text{m}^2/\text{s}^2$

## Solution to part (b)

- mass inflow and outflow are equal and one-dimensional, so

$$\begin{aligned}\dot{m} &= \rho_{\text{in}} A_{\text{in}} \dot{r}_{\text{in}} = \rho_{\text{out}} A_{\text{out}} \dot{r}_{\text{out}} \\ \implies A_{\text{out}} &= \frac{\rho_{\text{in}} A_{\text{in}} \dot{r}_{\text{in}}}{\rho_{\text{out}} \dot{r}_{\text{out}}} = \frac{v_{\text{out}} A_{\text{in}} \dot{r}_{\text{in}}}{v_{\text{in}} \dot{r}_{\text{out}}}\end{aligned}$$

- superheated steam tables give specific volumes, so

$$\begin{aligned}A_{\text{out}} &= \frac{(0.3\text{m}^3/\text{kg})(0.02\text{m}^2)(300\text{m/s})}{(0.405\text{m}^3/\text{kg})(155.6\text{m/s})} \\ &= 0.0286\text{m}^2\end{aligned}$$



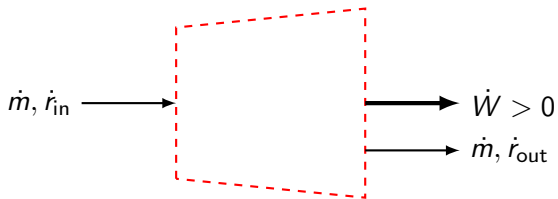
# Outline

Exam reminders

Nozzles and diffusers

**Turbines, compressors and pumps**

# Turbines



- turbines change the state of a working fluid to produce power

## Typical assumptions for turbines

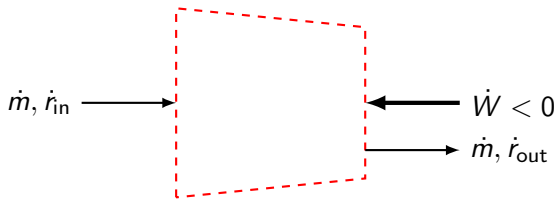
- steady state
- one-dimensional flow
- no change in PE (except for some hydro turbines)
- no change in KE (except for hydro and wind turbines)
- under these assumptions, steam and gas turbines satisfy

$$\dot{W} = \dot{Q} + \dot{m}(h_{\text{in}} - h_{\text{out}})$$

- if heat transfer is negligible ( $\dot{Q} = 0$ ), then

$$\dot{W} = \dot{m}(h_{\text{in}} - h_{\text{out}})$$

# Compressors and pumps



- compressors and pumps are 'backwards turbines'
- they consume power to change the state of a working fluid
- working fluid is a gas in compressors, liquid in pumps

## Typical assumptions for compressors

- steady state
- one-dimensional flow
- no change in PE
- no change in KE
- under these assumptions, compressors satisfy

$$\dot{W} = \dot{Q} + \dot{m}(h_{\text{in}} - h_{\text{out}})$$

- if heat transfer is negligible ( $\dot{Q} = 0$ ), then

$$\dot{W} = \dot{m}(h_{\text{in}} - h_{\text{out}})$$

## Typical assumptions for pumps

- steady state
- one-dimensional flow
- under these assumptions, pumps satisfy

$$\dot{m} \left[ \frac{1}{2}(\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) + g(z_{\text{in}} - z_{\text{out}}) + h_{\text{in}} - h_{\text{out}} \right] = \dot{W} - \dot{Q}$$

- if heat transfer is negligible ( $\dot{Q} = 0$ ), then

$$\dot{m} \left[ \frac{1}{2}(\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) + g(z_{\text{in}} - z_{\text{out}}) + h_{\text{in}} - h_{\text{out}} \right] = \dot{W}$$

## Example

Air enters a compressor through  $0.1 \text{ m}^2$  at  $290 \text{ K}$ ,  $1 \text{ bar}$  and  $6 \text{ m/s}$ . Air exits at  $450 \text{ K}$ . The compressor loses  $3 \text{ kW}$  to the surroundings via heat transfer. Find the compressor power.

# Given and find

- **given:**

- ◇  $A_{\text{in}} = 0.1 \text{ m}^2$ ,  $\dot{r}_{\text{in}} = 6 \text{ m/s}$
- ◇  $p_{\text{in}} = 1 \text{ bar}$ ,  $T_{\text{in}} = 290 \text{ K}$
- ◇  $T_{\text{out}} = 450 \text{ K}$
- ◇  $\dot{Q} = -3 \text{ kW}$

- **find:**

- ◇  $\dot{W}$



# Assumptions and basic equations

- **assume:**

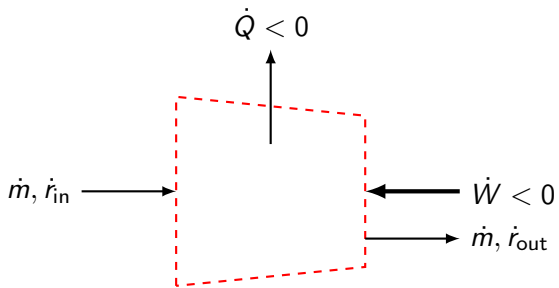
- ◇ steady state
- ◇ one-dimensional flow ( $\dot{m} = \rho A \dot{r}$ )
- ◇ no change in PE ( $z_{\text{out}} = z_{\text{in}}$ )
- ◇ no change in KE ( $\dot{r}_{\text{out}} = \dot{r}_{\text{in}}$ )
- ◇ ideal gas ( $p v = R T$ )

- **basic equations:**

- ◇ steady-state, single-inlet single-outlet 1st law:

$$\dot{m} \left[ \frac{1}{2} (\dot{r}_{\text{in}}^2 - \dot{r}_{\text{out}}^2) + g(z_{\text{in}} - z_{\text{out}}) + h_{\text{in}} - h_{\text{out}} \right] = \dot{W} - \dot{Q}$$

# System diagram



# Solution

- from the 1st law in steady state,

$$\dot{W} = \dot{Q} + \dot{m}(h_{\text{in}} - h_{\text{out}})$$

- because flow is one-dimensional,

$$\dot{m} = \frac{A_{\text{in}} \dot{r}_{\text{in}}}{v_{\text{in}}}$$

- from the ideal gas law,  $v_{\text{in}} = RT_{\text{in}}/p_{\text{in}}$ , so

$$\dot{W} = \dot{Q} + \frac{p_{\text{in}} A_{\text{in}} \dot{r}_{\text{in}} (h_{\text{in}} - h_{\text{out}})}{RT_{\text{in}}}$$

## Solution (continued)

- ideal gas table for air gives specific enthalpies:

Temp. [K]	h [kJ/kg]
290	290.1
450	452.0

- individual gas constant for air is  $R = 0.287 \text{ kJ}/(\text{kg K})$ , so

$$\begin{aligned}\dot{W} &= \dot{Q} + \frac{p_{\text{in}} A_{\text{in}} \dot{r}_{\text{in}} (h_{\text{in}} - h_{\text{out}})}{RT_{\text{in}}} \\ &= -3\text{kW} + \frac{(101\text{kPa})(0.1\text{m}^2)(6\text{m/s})(290\text{kJ/kg} - 452\text{kJ/kg})}{(0.287\text{kJ}/(\text{kg K}))(290\text{K})} \\ &= -118.0\text{kW}\end{aligned}$$

- since  $\dot{W} < 0$ , surroundings do work on compressor